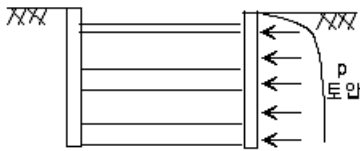


11장 토 압

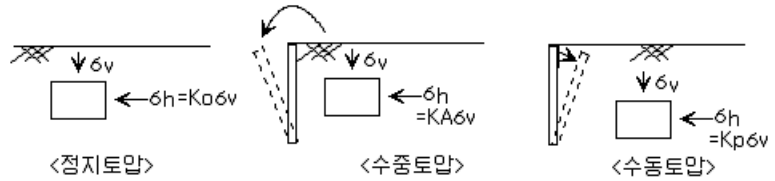
~흙막이 구조물에 작용하는 하중을 계산하기 위한 수평방향의 하중이다.

ex) 옹벽, (가설)흙막이벽, 지중지하벽



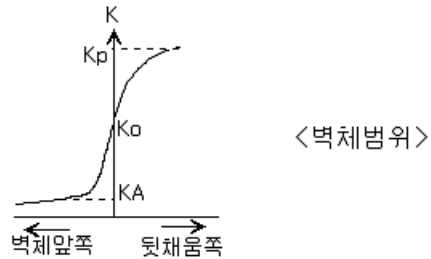
11.2 토압의 종류

- ① 정지 토압 = K_0
- ② 주동 토압 = K_a
- ③ 수동 토압 = K_p



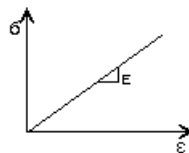
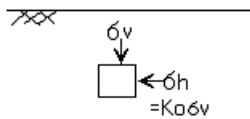
· 토압계수

$$K = \frac{\sigma_h}{\sigma_v}$$

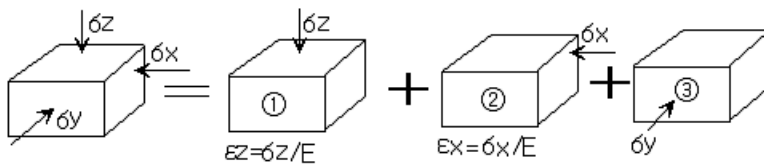


11.3 정지 토압계수

-지반을 탄성체로 가정 → Hook's law를 따른다.



-중첩의 원리 적용가능



※ 포이송비

Hook's law: $\sigma = E\epsilon_a$ 여기서, $\epsilon_a = \frac{dl}{l}$

$\mu = -\frac{\epsilon_l(\text{횡변형율})}{\epsilon_a(\text{축변형율})}$ (정의) → $\epsilon_l = -\mu\epsilon_a = -\mu\frac{\sigma}{E}$

$$\begin{aligned} \varepsilon_z &= \frac{\sigma_z}{E} \sigma & \varepsilon_x &= \frac{\sigma_x}{E} & \varepsilon_y &= \frac{\sigma_y}{E} \\ \varepsilon_x &= -\mu \varepsilon_z = \left(-\mu \cdot \frac{\sigma_z}{E}\right) & \varepsilon_y &= -\mu \cdot \frac{\sigma_x}{E} & \varepsilon_x &= -\mu \cdot \frac{\sigma_y}{E} \\ \varepsilon_y &= -\mu \varepsilon_z = -\mu \cdot \frac{\sigma_z}{E} & \varepsilon_t &= -\mu \cdot \frac{\sigma_x}{E} & \varepsilon_z &= -\mu \cdot \frac{\sigma_y}{E} \end{aligned}$$

$$\begin{aligned} \rightarrow \varepsilon_x &= \frac{1}{E} [\sigma_x - \mu(\sigma_y + \sigma_z)] \\ \rightarrow \varepsilon_y &= \frac{1}{E} [\sigma_y - \mu(\sigma_x + \sigma_z)] \\ \rightarrow \varepsilon_z &= \frac{1}{E} [\sigma_z - \mu(\sigma_x + \sigma_y)] \end{aligned}$$

· 정지토압조건

→ $\varepsilon_x = \varepsilon_y = 0$ 인 조건에 해당

윗식에 대입

$$\sigma_x = \mu(\sigma_y + \sigma_z)$$

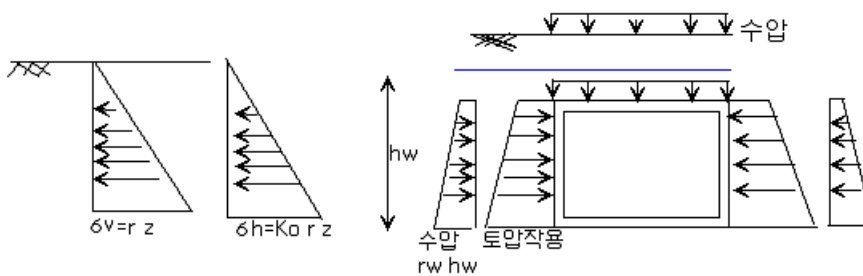
$$\sigma_y = \mu(\sigma_x + \sigma_z) \text{ 위 식에 대입 } \rightarrow \sigma_x = \frac{(1+\mu)\mu}{1-\mu^2} \cdot \sigma_z$$

$$\therefore \sigma_x = \frac{\mu}{1-\mu} \cdot \sigma_z \quad \therefore K_o = \frac{\mu}{1-\mu}$$

-Jacky 공식 (경험공식)

for 사질토 → $K_o = 1 - \sin\phi'$

for 점성토 → $K_o = (1 - \sin\phi') \sqrt{O.C.R}$ ($O.C.R = \frac{\sigma'_c}{\sigma'_{v0}}$)

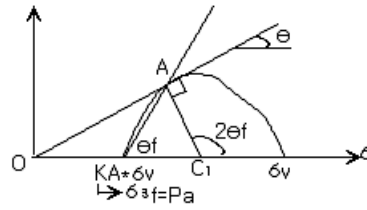
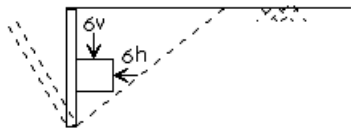


11.4 Rankine의 토압이론

→ 벽면 마찰각을 무시한 토압이론

사질토 ($c=0$) 인 경우

i) 주동 토압

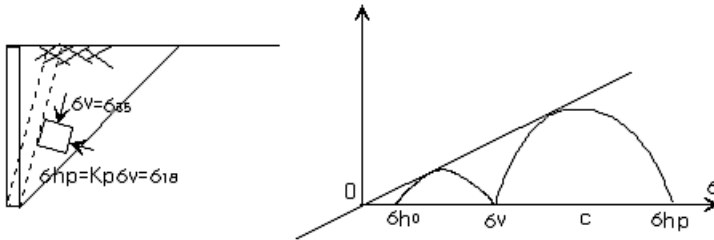


$$\sin\phi = \frac{CA}{OC} = \frac{\frac{(\sigma_v - \sigma_{ha})}{2}}{\frac{(\sigma_v + \sigma_{ha})}{2}} \rightarrow \frac{\sigma_{ha}}{\sigma_v} = \frac{1 - \sin\phi}{1 + \sin\phi} = \tan^2\left(45^\circ - \frac{\phi}{2}\right) = K_a$$

$$\therefore K_a = \frac{1 - \sin\phi}{1 + \sin\phi}$$

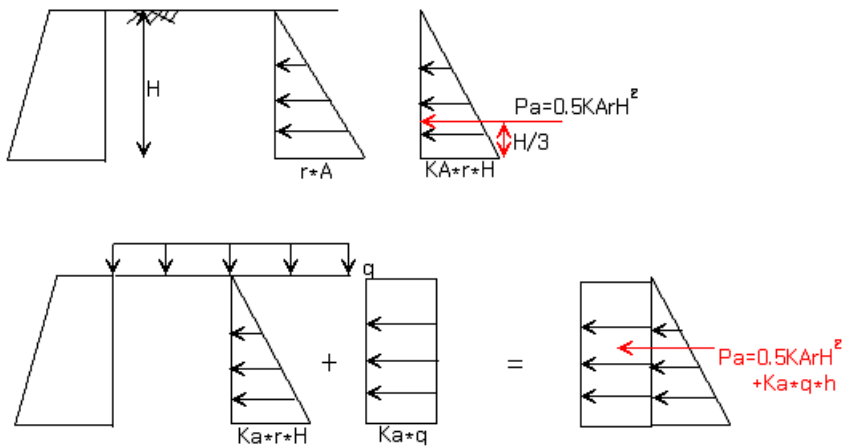
$$2\theta_f = 90^\circ + \phi \rightarrow \theta_f = 45 + \frac{\phi}{2}$$

ii) 수동 토압

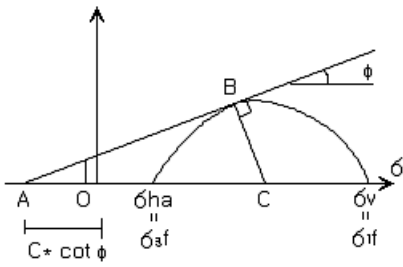


$$K_p = \frac{\sigma_{hp}}{\sigma_v} = \frac{1 + \sin\phi}{1 - \sin\phi} = \tan^2\left(45^\circ + \frac{\phi}{2}\right) = \frac{1}{K_a}$$

-주동 토압의 분포와 합력의 위치



2 점성토의 주동 및 수동토압(c≠0인 경우)



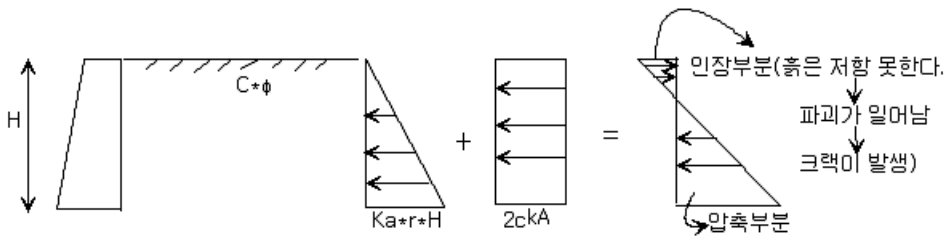
$$\sin \phi = \frac{CB}{AO + OC}$$

$$= \frac{(\sigma_v - \sigma_{ha})/2}{c \cdot \cot \phi + (\sigma_v + \sigma_{ha})/2}$$

$$\sigma_{ha} = \left(\frac{1 - \sin \phi}{1 + \sin \phi} \right) \sigma_v - 2 \cdot c \cdot \frac{\cos \phi}{1 + \sin \phi}$$

$$= K_a \cdot \gamma \cdot z - 2c \sqrt{K_a}$$

- 토압 분포



- 인장깊이 선정

$\sigma_{ha} = 0$ 인 시점

$$\sigma_{ha} = K_a \cdot \gamma \cdot Z_0 - 2C \sqrt{K_a} = 0$$

$$\therefore Z_0 = \frac{2C}{\gamma} \cdot \frac{1}{\sqrt{K_p}} = \frac{2C}{\gamma} \cdot \sqrt{K_p}$$

- 수동토압계수

$$\sigma_{hp} = K_p \cdot \gamma \cdot Z + 2C \sqrt{K_p} \quad \left(K_p = \frac{1 + \sin \phi}{1 - \sin \phi} \right)$$

-지표면이 경사진 경우에 대한 토압

$$\begin{aligned} \delta v &= W/b = Z \cdot b' \cdot \gamma \cdot \cos i / b' \\ &= \gamma Z \cdot \cos i \end{aligned}$$

$$K_a = \frac{\delta h a}{\delta v}$$

$$O A^2 = \delta v^2 \cdot \cos^2 i + \delta h a^2 \cdot \sin^2 i = \delta v^2 (\cos^2 i + \sin^2 i)$$

$$O A = \delta v$$

$$O B = \delta h a$$

$$K_a = \frac{O B}{O A} = \frac{O B - A D}{O D + A D}$$

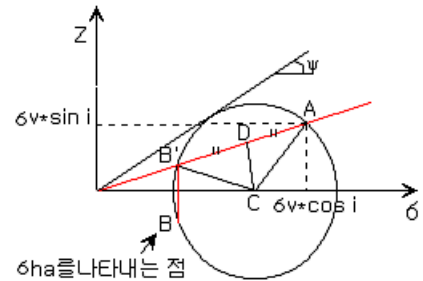
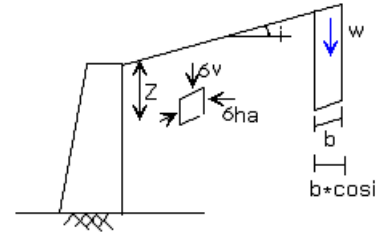
$$O D = O C \cdot \cos I$$

$$A D = \sqrt{A C^2 - C D^2} \quad (A C = O C \cdot \sin \psi, C D = O C \cdot \sin I)$$

$$\begin{aligned} \therefore K_a &= \frac{O C \cdot \cos i - \sqrt{O C^2 \cdot \sin^2 \phi + O C^2 \cdot \sin^2 i}}{O C \cdot \cos i + \sqrt{O C^2 \cdot \sin^2 \phi - O C^2 \cdot \sin^2 i}} = \frac{\cos i - \sqrt{\sin^2 \phi - \sin^2 i}}{\cos i + \sqrt{\sin^2 \phi - \sin^2 i}} \\ &= \frac{\cos i - \sqrt{\cos^2 i - \cos^2 \phi}}{\cos i + \sqrt{\cos^2 i - \cos^2 \phi}} = \frac{1}{K_p} \end{aligned}$$

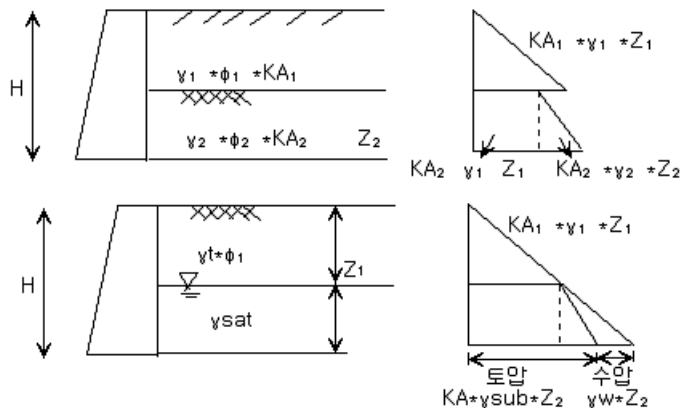
$$\delta h a = K_a \cdot \delta v = K_a \cdot \gamma \cdot z \cdot \cos i$$

$$\therefore P_a = \frac{1}{2} K_a \cdot \gamma \cdot H^2 \cdot \cos I$$



11.4 뒤채움이 이층이거나 지하수위가 있는 경우

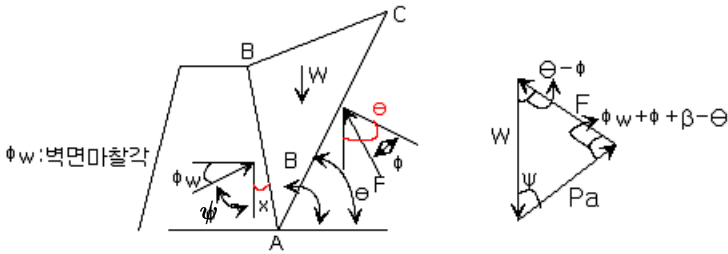
-주동토압



$$\begin{aligned} \gamma_{sub} &= \gamma_{sat} - \gamma_w \\ &= \frac{G_s - 1}{1 + e} \gamma_w \end{aligned}$$

11.5 Coulomb의 토압이론 : ~벽면에 마찰각을 고려한 토압이론

① $c=0$ 인 경우



$$x = 90 - (180 - \beta) = \beta - 90^\circ$$

$$\begin{aligned} \therefore \psi &= 90 - \phi_w - (\beta - 90) \\ &= 180 - (\beta + \phi_w) \end{aligned}$$

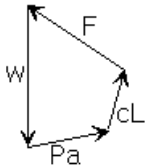
$$\frac{Pa}{\sin(\theta - \phi)} = \frac{W}{\sin(\phi + \phi_w + \beta - \theta)}$$

$$\therefore PA = W \cdot \frac{\sin(\theta - \phi)}{\sin(\phi + \phi_w + \beta - \theta)}$$

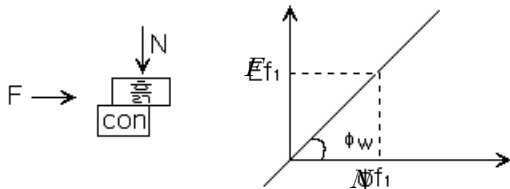
$$\frac{dPA}{d\theta} = 0 \text{ 일 때의 } \theta \text{ 값 추정}$$

$$PA = \frac{\gamma H^2}{2} \left[\frac{\sin(\beta - \phi) \csc \beta}{\sqrt{\sin(\beta + \phi_w) + \sqrt{\frac{\sin(\phi + \phi_w) \cdot \sin(\phi - \theta)}{\sin(\beta - \theta)}}}} \right]^2$$

② $c \neq 0$ 인 경우



-벽면 마찰각 (ϕ_w)



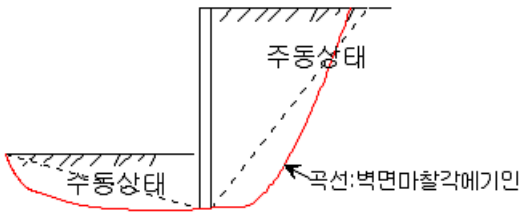
\therefore 일반적으로는 $\phi_w = \frac{2}{3} \phi$ 로 가정

11.6 실제 활동면의 현상

-수동토압의 경우 $\phi_w > \frac{\phi}{3}$ 이면

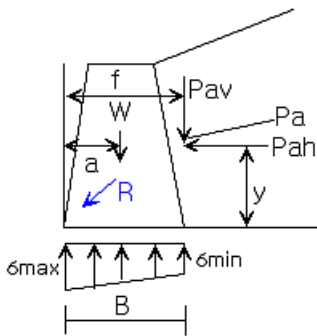
실제 수동토압과 현저한 차이 발생

→ 직선 파괴 가정 = 수동토압의 크기를 실제 보다 크게 평가



11.7 옹벽의 안정

1. 안정조건



①수평활동에 대한 안정

$$F_s = \frac{\text{수평저항력}}{\text{수평활동력}} = \frac{Ff}{Rh} = Rv \cdot \frac{\tan\phi_w}{Rh} > 1.5$$

②전도에 대한 안정

$$F_s = \frac{M_r(\text{저항모멘트})}{M_o(\text{활동모멘트})} = \frac{W \cdot a + Pav \cdot f}{Pah \cdot y} > 1.5$$

③허용지지력 검토

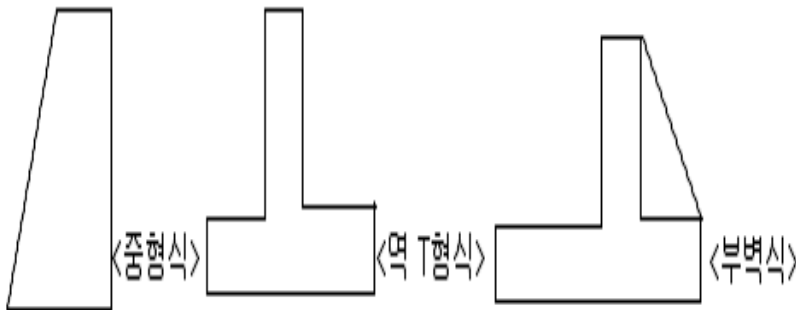
$$F_s = \frac{qu}{\sigma_{\max}} > 3.0$$

*편심

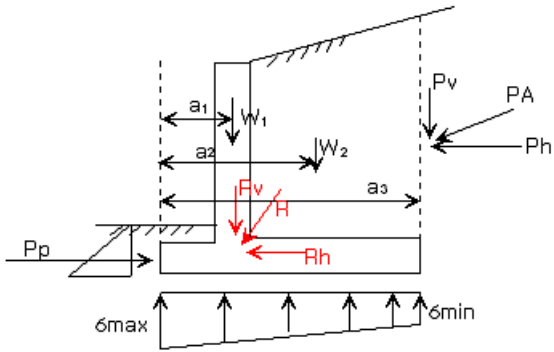
$$\frac{M}{I} \cdot y = \frac{Rv \cdot e}{\frac{1}{12} \cdot B^3} \cdot \left(\frac{B}{2}\right) = \frac{6Rv \cdot e}{B^2}$$

$$\therefore \sigma = \frac{Rv}{B} \left(1 \pm \frac{6e}{B}\right)$$

-옹벽의 종류



(가상벽면에 토압작용)



-Rankine 토압이론을 적용

①옹벽의 수평활동안정

$$F_s = \frac{R_v \cdot \tan \phi_w}{R_h (= P_h)} > 1.5$$

②전도활동에 대한 안정

$$F_s = \frac{\text{저항모멘트}}{\text{활동모멘트}} = \frac{W_1 a_1 + W_2 a_2}{P_h y - P_v a_3} > 1.5$$

③허용지지력에 대한 안정

$$F_s = \frac{qu}{\sigma_{\max}} > 3 \quad \left(qa(\text{허용지지력}) = \frac{qu}{3} (\text{극한지지력}) \right)$$

$$\therefore \sigma = \frac{R_v}{B} \left(1 \pm \frac{6e}{B} \right)$$

- $\sigma_{\min}=0$ 인 조건에서

$$\rightarrow 1 - \frac{6 \cdot e}{B} = 0 \text{인 지점} \rightarrow e = \frac{B}{6}$$

σ_{\min} 값이 -값이 되면 인장력 발생

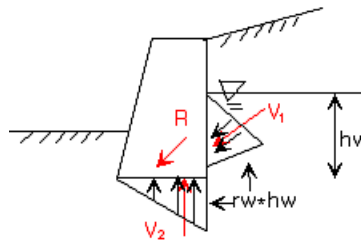
지반 반력에서 인장력이 발생하지 않도록 하기 위한 최대편심 거리는 $B/6$ 이다.

(편심이 $B/3$ 안에 존재해야 한다.)

2.지하수위가 옹벽의 안정에 끼치는 영향

-활동에 대한 안전율

$$F_s = \frac{(R_v - V_2) \tan \phi_w}{R_h + V_{1h}} > 1.5$$



3.옹벽에 작용하는 간이 토압분포

-by Terzaghi, Peck (단, 옹벽높이가 6m이내일 때)

$$P_h = \frac{1}{2} K_h \cdot H^2$$

$$P_v = \frac{1}{2} K_v \cdot H^2 \quad (i=0 \text{이면 } \rightarrow P_v=0) \rightarrow K_v=0$$

<도표이용>

